

**METHOD AND APPARATUS FOR OPERATING AN  
ELECTROCHEMICAL FUEL CELL**

**Cross-Reference to Related Application**

This application is related to and claims priority benefits from U.S. Provisional Patent Application Serial No. 60/253,824 filed November 29, 2000, entitled "Method And Apparatus For Operating An Electrochemical Fuel Cell". The '824 provisional application is incorporated herein by reference in its entirety.

10 **Field of the Invention**

The present invention relates to a method and apparatus for operating an electrochemical fuel cell, such as, for example, to increase the life or durability of the cell.

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**Background of the Invention**

Electrochemical fuel cells convert fuel and oxidant fluid streams to electricity and reaction product. Solid polymer electrochemical fuel cells generally employ a membrane electrode assembly (MEA) comprising a solid polymer electrolyte or ion-exchange membrane disposed between two porous electrically conductive electrode layers. An electrocatalyst is typically disposed at each membrane/electrode layer interface to induce the desired electrochemical reaction.

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In typical fuel cells, the MEA is disposed between two electrically conductive separator plates. A fluid flow field provides a means for directing the fuel and oxidant to the respective electrocatalyst layers, specifically, at the anode on the fuel side and at the cathode on the oxidant side. A simple fluid flow field may consist of a chamber open to an adjacent porous electrode layer with a first port serving as a fluid inlet and a second port serving as a fluid outlet. The fluid flow field may be the porous electrode layer itself. More complicated fluid flow fields incorporate at least one fluid channel between the inlet and the outlet for directing the fluid stream in contact with the electrode layer or a guide barrier for controlling the flow path of the reactant through the flow field. The fluid flow field is commonly integrated with the separator plate by locating a plurality of open-faced channels on the faces of the separator plated facing the electrodes. In a single cell arrangement, separator plates are provided on each of the anode and cathode sides.

The plates act as current collectors and provide structural support for the electrodes.

The fuel stream directed to the anode by the fuel flow field migrates through the porous anode and is oxidized at the anode electrocatalyst layer. The oxidant stream directed to the cathode by the oxidant flow field migrates

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through the porous cathode and is reduced at the cathode electrocatalyst layer.

Solid polymer fuel cells generally use fuels, such as, for example, hydrogen or methanol, which are oxidized at the anode to produce protons. The protons migrate through the ion-conducting electrolyte membrane and react with an oxidant such as oxygen in the air at the cathode to produce water as a reaction product.

Two or more fuel cells can be connected together, generally in series but sometimes in parallel, to increase the overall power output of the assembly. In series arrangements, one side of a given plate can serve as an anode plate for one cell and the other side of the plate can serve as the cathode plate for the adjacent cell.

Such a series connected multiple fuel cell arrangement is referred to as a fuel cell stack, and is typically held together in its assembled state by tie rods and end plates. Apart from being provided with inlets and outlets for the oxidant and fuel streams, the fuel cell stack is typically also provided with a coolant inlet and outlet for the flow of a coolant through the stack.

During operation of a fuel cell various failures or problems can occur which limit the useful life or durability and ultimately the reliability of the cell. For instance, leaks may develop in the ion-exchange membrane (allowing

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the fuel and oxidant reactants to transfer over to the wrong electrodes) or in the various other fluid seals in the fuel cell. Failures may also occur due to build up of contaminants that  
5 collect in the fuel cell.

The types of failure which occur, resulting in declining performance of the cell or failure or breakdown of the cell, and the average time period within which such failure or failures  
10 occur can be determined experimentally for a particular type of cell or for a selected number of such cells and then averaged. This time period, whether determined for a single cell or for a selected number of cells, for which the  
15 mean value (sometimes referred to as the average value) is then obtained under conventional operating conditions is referred to herein as "mean life expectancy" or "mean time to failure" (MTTF).

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#### Summary of the Invention

An improved method operates a fuel cell or a fuel cell stack supplied with a fluid stream. The fuel cell has a mean life expectancy that may  
25 be determined empirically. The method comprises the step of reversing the direction of flow of the fluid stream after a time period of operation of the fuel cell, the time period being less than the mean life expectancy of the cell. The time  
30 period has a value that is a substantial part of

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the value of the mean life expectancy. A  
"substantial part" will typically be more than  
half of the mean life expectancy but may mean 1%  
or less of the mean life expectancy. In the  
5 present methods, the fluid flow stream is not  
reversed every few minutes but only after  
operating a substantial portion of the mean life  
expectancy. The method is useful in increasing  
fuel cell life or durability, particularly that  
10 of a solid polymer electrolyte fuel cell.

The reversed fluid stream may be either one  
or both of the fuel and oxidant reactant streams,  
thereby resulting in a flow reversal of one or  
both the reactants through their respective  
15 reactant flow fields in the fuel cell. Where  
applicable, the reversed fluid stream may be a  
coolant stream, thereby resulting in a flow  
reversal of coolant through a coolant flow field.

Reversing the fluid flow direction may  
20 change the location at which the greatest amount  
of degradation occurs for a given degradation  
mechanism, thereby delaying the onset of a fuel  
cell failure. The method may desirably be  
employed once (for instance, after the fuel cell  
25 has been operated for about 75% to about 90% of  
its mean life expectancy) or multiple times  
during the life of the fuel cell. However, a  
modest number of fluid flow direction reversals  
is preferred (for instance, less than about 10  
30 times during the life of the fuel cell).

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The flow of the fluid stream may be reversed simply by switching the inlet/outlet functions of the ports, for example, by disconnecting the supply and exhaust conduits from the first port and second ports, respectively, and then connecting the supply and exhaust conduits to the second and first ports, respectively. This may be performed manually or using an appropriate automated subsystem. Where appropriate, fluid flow may be exhausted or dead-ended at or beyond the second port instead. The fuel cell may be designed such that it is symmetric about the first and second ports in which case the fluid flow may be reversed by rotating the fuel cell to align the second and first ports with the supply and exhaust conduits respectively after the disconnecting step.

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Detailed Description of Preferred Embodiment(s)

It has been found that certain degradation mechanisms in fuel cells occur at rates that vary greatly with respect to the location of the working  
5 fluid inlets and/or outlets. For instance, the current densities in the regions of the fuel and oxidant reactant inlets are higher than those in the regions of the outlets in solid polymer electrolyte fuel cells. This can make enough  
10 difference to the material degradation rates in the inlet regions that related material failures may occur predominantly in the inlet regions. Similarly, cell temperature is relatively higher in the region of the reactant outlets in such cells.  
15 This can cause higher rates of temperature related seal material degradation in the outlet regions. Further, contaminants in the supplied reactant streams also tend to accumulate mainly in the inlet areas of the fuel cell, eventually resulting in a  
20 significant reduction in fuel cell performance. However, the reduction in performance is more significant than it would be if the contaminants instead had collected at the outlet areas because the inlet areas are the regions operating at the  
25 greatest current density.

To illustrate the variation of degradation with inlet/outlet location, a conventional solid polymer electrolyte fuel cell stack comprising 25 individual fuel cells was operated for about 12,000  
30 hours on reformat fuel and air oxidant supplies.

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A small amount of air (2%) was admitted to the supplied fuel stream to prevent carbon monoxide poisoning of the anode catalyst. The stack was operated at full reactant pressures and power

5 output for half of the testing period. However, by that time, many leaks developed within the stack, resulting in significant mixing of the fuel and oxidant streams within the stack. Also, the reactant fluid manifolds developed leaks at the

10 seals, resulting in significant loss of reactant to the surrounding environment. Consequently, the stack could only be operated at reduced reactant pressures and hence at a half power output condition for the last half of the testing period.

15 The stack was then disassembled and the cells analyzed for the location and frequency of the various leak types.

In the Table 1 below, the number of cells in the stack is tabulated in which a particular leak

20 and location was observed.

### Table 1

Leak type and location <sup>a</sup>	# cells with leak
membrane leak near oxidant outlet	20
membrane leak near oxidant inlet	1
membrane leak near fuel outlet	3
membrane leak near fuel inlet	17
glue joint seal leak near oxidant outlet	17
glue joint seal leak near oxidant inlet	0
glue joint seal leak near fuel outlet	5
glue joint seal leak near fuel inlet	0

5           As is evident from the foregoing data, the frequency of the various leak types varies greatly with location relative to the reactant inlets and outlets. As such, switching the inlet and outlet positions (by reversing reactant flow through the relevant flow field) may be expected to reduce the degradation rate in the more degraded regions at the expense of increasing the degradation rate in the less degraded regions. This however should postpone the onset of leaks or cell failures by averaging out the accumulated degradation over the affected cell component, thereby increasing cell

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FIG. 1 illustrates, in exploded view, a solid polymer electrolyte fuel cell stack 10, including a pair of end plates assemblies 15, 20 and a plurality of fuel cell assemblies 25. Tie rods 30 extend between end plates 15 and 20 to retain and secure stack 10 in its assembled state with fastening nuts 32. Springs 34 threaded on the tie rods 30 interposed between the fastening nuts 32 and the end plate 20 apply resilient compressive force to the stack in the longitudinal direction. Reactant and coolant fluid streams are supplied to and exhausted from internal manifolds and passages in the stack 10 via stack inlet and outlet ports in end plates 15 and 20. In FIG. 1, the fuel stream is supplied by supply conduit 50 to fuel inlet port 52 (The conduits and ports are shown in disconnected form in FIG. 1, but connected during operation) and is exhausted out exhaust conduit 54 from fuel outlet port 56. (The oxidant fuel stream and coolant stream plumbing are not shown in FIG. 1.) Fuel

cell stack 10 is symmetric about ports 52, 56 and  
conduits 50, 54 in that ports 56 and 52 can be  
aligned with conduits 50 and 54 respectively by  
rotating stack 10 about an axis normal to end  
5 plate 20. As shown by the exploded portion of  
FIG. 1, each fuel cell assembly 25 includes an  
anode flow field plate 35, a cathode flow field  
plate 40, and a membrane electrode assembly 45  
interposed between plates 35 and 40. Membrane  
10 electrode assembly 45 comprises an ion-exchange  
membrane interposed between an anode and a  
cathode. Plate 35 has a plurality of fluid flow  
channels 35a formed in its major surface facing  
membrane electrode assembly 45 for directing a  
15 reactant stream in contact with one of the  
electrodes of membrane electrode assembly 45.

Reversal of the flow direction of any of the  
working fluids supplied to stack 10 may be  
accomplished manually at appropriate times during  
20 its life. For instance, to effect a reversal of  
the fuel flow direction, supply conduit 50 and  
exhaust conduit 54 may be disconnected from ports  
52 and 56 respectively and then repositioned and  
reconnected in the opposite order (that is, to  
25 ports 56 and 52 respectively). Alternatively,  
after disconnecting, the entire stack 10 may be  
rotated about an axis normal to end plate 20 such  
that supply conduit 50 and exhaust conduit 54 now  
align with ports 56 and 52 respectively. In this  
30 way, conduits 50 and 54 do not need to be

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repositioned.

An alternative embodiment is shown in FIGs. 2a and 2b, which schematically depict a fuel cell stack 100 that has two fuel stream ports 110, 120 and associated manifolds 115, 125 for supplying and exhausting a fuel stream to and from individual fuel cells in stack 100. Lines 130 represent the individual fuel flow fields through which the fuel stream is directed to the anodes.

In the illustrated embodiment, the fuel flow fields of individual fuel cells of the stack are manifolded in parallel; however, some or all of them may be manifolded in series. Stack 100 also has ports, and manifolds (not shown) for supplying and exhausting an oxidant stream to and from oxidant flow fields of stack 100. It also has ports and manifolds (not shown) for the flow of coolant through the cell.

In FIG. 2a, port 110 initially acts as the fuel stream inlet and manifold 115 supplies fuel stream to flow fields 130. Port 120 initially acts as the outlet for exhausting a fuel stream from flow fields 130 and manifold 125.

Container 140 supplies a fuel stream (such as hydrogen) to stack 100 via a fuel stream flow switch 150. Fuel stream flow switch 150 controls the directional flow of the fuel stream through stack 100 by controlling which one of ports 110, 120 acts as the fuel stream inlet for flow fields 130.

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In FIG. 2a, fuel stream flow switch 150 is set to direct the fuel supply stream via port 110 and exhaust the fuel stream from the fuel cells through port 120. In FIG. 2b, fuel stream flow switch 150 is set so that port 120 acts as the fuel stream inlet, and port 110 acts as the fuel stream outlet. The arrows on lines 130, represent the direction of fuel stream flow through the individual fuel cell fuel flow fields. Accordingly, the arrows on lines 130 indicate that the fuel stream flow direction through the fuel cell fuel flow fields has reversed from FIG. 2a to FIG. 2b.

In FIGs. 2a and 2b, fuel stream flow switch 150 is represented by a single component. However, as will be appreciated by those skilled in the art, fuel stream flow switch 150 may be any device or combination or assembly of components capable of reversing the direction of fluid flow through the fuel flow fields 130. For example, the fuel stream flow switch 150 may comprise various valves cooperatively operated.

In FIGs. 2a and 2b, fuel stream flow switch 150 is schematically depicted as a device with a sliding motion for selecting a setting for controlling the fuel stream flow direction. However, any known type of flow switch or apparatus can be used, for example, one that uses a rotary motion or a pivoting motion.

Since the flow switching generally may be

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the three streams may be reversed.

The method of reversal of fluid flow may be employed to counteract failure of a fuel cell or to prolong the time before a failure occurs. Those  
5 skilled in the art will appreciate that numerous options exist for the number and timing of the flow reversals in order to achieve these benefits. Generally, however, the number of reversals performed during the lifetime of the fuel cell is  
10 preferably kept small (for example, less than about 10) since the lifetime gain obtained with each additional reversal is expected to diminish. Thus, the lifetime gain associated with more numerous reversals may not offset the inconvenience of  
15 additional manual switching operations or the additional cost and potential reliability issues associated with more automated switching. Reversals are preferably performed after operating for a time period that is substantial compared to  
20 the mean life expectancy of the fuel cell. For example, the life of a fuel cell stack may be limited by the membrane degrading at a faster rate at the fuel inlet, than in the rest of the cell. The average or mean time period at which this  
25 failure occurs can be obtained empirically. If the mean time to failure is found to be 6500 hours, then a fuel flow switch (such as device 150 in FIGs. 2a and 2b) may be operated to switch the fuel inlet and outlet at 5000 hours. In this way the  
30 useful life of the cell is prolonged. Similarly,

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this method can be applied to counteract or delay failures associated with oxidant flow or coolant flow.

While particular elements, embodiments and applications of the present invention have been shown and described, it will be understood, of course, that the invention is not limited thereto since modifications may be made by those skilled in the art, particularly in light of the foregoing teachings. It is therefore contemplated that the appended claims cover such modifications that incorporate those features coming within the scope of the invention.

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